### BINDURA UNIVERSITY OF SCIENCE EDUCATION

#### **FACULTY OF SCIENCE AND ENGINEERING**

**AEH 308** 

### Department Of Engineering and Physics Bachelor of Science (Honours) in Agricultural Engineering Food Engineering

3 HOURS (100 MARKS)

### **INSTRUCTIONS**

APR 2025

Answer any FOUR questions. Each question carries 25 marks.

### Question 1

- a. Calculate the component mass balance for mixing ingredients to make 18 kg of beef sausages having a fat content of 25%, using fresh beef meat and beef fat. Typically, beef meat contains 15% protein, 10% fat and 73% water and beef fat contains 82% fat, 10% water and 6% protein.

  [6 marks]
- b. A 5 cm inside diameter pipe is being used to pump liquid food into a buffer tank of 2.5 m diameter and 3.5 m height. If the density of the liquid is 1250 kg/m³ and viscosity is 1540x10<sup>-6</sup> Pa s, calculate time to fill the tank under laminar conditions in the pipe.
   [9 marks]
- c. Briefly describe five functional properties of ingredients used in meat processing. [10 marks]

### Question 2

- a. With the aid of practical examples, explain how the distillation process is used to achieve great purity. [8 marks]
- b. Calculate the temperature of tomato juice (density = 995 kg/m³) in a steam jacketed hemispherical kettle of 0.8 m radius after 4 min. of heating. It is given that the initial temperature of tomato juice is 18°C, surface temperature of the kettle is 70°C and the convective heattransfer coefficient in the steam jacket is 6500 W/(m²°C). Assume a specific heat of tomato juice of 4.12 kJ/(kg°C). [8 marks]
- c. Calculate the freezing time of a spherical food product being frozen in an air-blast freezer using Plank's equation. It is given that the initial product temperature is 15°C, cold air is (-)35°C, the product has a 12 cm diameter with density of 1050 kg/m³, the initial freezing temperature is (-)3°C, the thermal conductivity of the frozen product is 1.65 W/(m K), heat transfer coefficient is 82 W/(m²K) and the latent heat of fusion is 320 kJ/kg. [9 marks]

### Question 3

- a. With the aid of diagrams, describe the essential operational differences between co-current and counter-current modes of continuous extraction processes.

  [12 marks]
- b. Bran flakes (MC<sub>wb</sub> 80%) are being dried in a concurrent flow drier. The moisture content of the air entering the drier is 0.07 kg of water per 1 kg dry air. The moisture content of air leaving the drier is 0.20 kg water per 1 kg of dry air. The air flow rate in the drier is 130 kg dry air per hour.

If 65 kg of wet bran flakes enter the drier per hour at a steady state, calculate: [5 marks] i. the mass flow rate of dried bran, ii. the  $MC_{db}$  of dried bran exiting the drier. [8 marks] Question 4 a. With the aid neat sketches, explain the principle of operation of the following types of solid particle size reduction equipment: [5 marks] Hammer mill. [5 marks] Attrition mill. b. A liquid food (specific heat =  $6.5 \text{ kJ/[kg }^{\circ}\text{C]}$ ) flows in the inner pipe of a double pipe heat exchanger. The liquid food enters the heat exchanger at 25°C and exits at 70°C. The flow rate of the liquid food is 1.2 kg/s. In the annular section, hot water at 98°C enters the heat exchanger and flows counter-currently at a flow rate of 1.8 kg/s. Assuming steady-state conditions, if the average specific heat of water is 4.18 kJ/(kg °C), calculate: [5 marks] the exit temperature of water, i. [5 marks] log-mean temperature difference, ii. the length of the heat exchanger when the average overall heat iii. transfer coefficient is 1800 W/(m<sup>2</sup> °C) and the diameter of the inner [5 marks] pipe is 8 cm. Question 5 a. An air-vapor mixture is at 20°C and 50% relative humidity. Using the psychrometric chart, determine: [1 mark] the wet bulb temperature, i. [1 mark] humidity ratio, ii. [1 mark] specific volume, iii. [1 mark] enthalpy, and iv. [1 mark] dew-point temperature. b. Calculate the rate of thermal energy required to heat  $6.5 \; \text{m}^3/\text{ s}$  of outside air at 30°C dry bulb temperature and 80% relative humidity to a [8 marks] dry bulb temperature of 80°C. c. In fruit juice processing, apple juice is preserved at room temperature by treatment with SO<sub>2</sub>. It is desired to strip some of the SO<sub>2</sub> from the sulphured juice. The stripping of the juice will be carried out with a counter-current flow of air in a tray column. The air has a temperature of 20°C and contains water vapour at equilibrium with liquid juice at this temperature. The juice flow rate is 0.82m<sup>3</sup>s<sup>-1</sup>. The SO<sub>2</sub> concentration in juice (mole fraction) is to be reduced from 10<sup>-4</sup> to 10<sup>-7</sup>. The initial and final concentrations of  $SO_2$  in air are  $y_i=0$  and  $y_o=0.6x10^{-3}$  (mole fraction). If the partitioning coefficient is 5 (mole fraction  $c_e/c_r$  basis), calculate: [4 marks] the air flow rate, i. [3 marks] separation factor (S) and ii. [5 marks] the number of equilibrium stages. iii.

### Question 6

a. Briefly explain three factors that affect the duration of completely frying foods.

[6 marks]

b. Calculate the size of the motor required to avocado oil and sunflower oil in a ratio of 1 to 4 by a propeller agitator 25 cm in diameter operating at 1200 rpm in a cylindrical tank of 1 m diameter at 25°C. It is given that P<sub>o</sub> is 0.7, the viscosity of avocado oil at 25°C is 0.09 Nsm<sup>-2</sup>, the density of avocado oil 860 kg m<sup>-3</sup>, the viscosity of sunflower oil 0.2 Nsm<sup>-2</sup> and the density of rapeseed oil 920 kg m<sup>-3</sup>.

[9 marks]

c. An 8 kW oven has a hearth area of 4 m² and operates at 210°C. It is loaded with two batches of bread dough in baking tins; 150 loaves on the first batch and 120 loaves on the second batch. The surface of each loaf measures 12 cm x 20 cm. Assuming that the emissivity of dough is 0.85, that the dough bakes at 100°C, and that 90% of the heat is transmitted in the form of radiant energy, calculate the efficiency of energy use for each batch.

[10 marks]

End of paper

# **FOOD ENGINEERING (AEH308)**

## MATHEMATICAL FORMULAE

### GRINDING AND CUTTING

$$dE/dL = KL^n$$

Kick

 $K = K_{\rm K} f_{\rm c}$ 

 $dE/dL = K_{\rm K} f_{\rm c} L^{-1}$ 

 $E = K_{\rm K} f_{\rm c} \log_{\rm e}(L_1/L_2)$ 

[law]

Rittinger

 $K = K_{\rm R} f_{\rm c}$ 

 $\mathrm{d}E/\mathrm{d}L = K_{\mathrm{R}}f_{\mathrm{c}}L^{-2}$ 

 $E = K_{\rm R} f_{\rm c} (1/L_2 - 1/L_1)$ 

[law]

Bond

 $E = E_1 (100/L_2)^{1/2} [1 - (1/q^{1/2})]$  [Iaw]

 $q = L_1/L_2$ 

# Modification of the grinding energy equations

Energy required E (kWh/kg) for reducing particle size from  $x_1$  to  $x_2$ 

Rittinger

$$E = K_R \left( \frac{1}{x_2} - \frac{1}{x_1} \right)$$

Kick

$$E = K_k \ln \left( \frac{x_1}{x_2} \right)$$

Bond

$$E = K_B \left[ \left( \frac{1}{x_2} \right)^{\frac{1}{2}} - \left( \frac{1}{x_1} \right)^{\frac{1}{2}} \right]$$

EXTRACTION WASHING LEACHING

VASHING

$$\alpha = \frac{Ce}{Cr}$$

 $\Phi_{\text{VfCf}} + \Phi_{\text{VsCs}} = \Phi_{\text{VeCe}} + \Phi_{\text{VrCr}}$ 

 $\frac{\text{Amount extracted}}{\text{Amount in raffinate}} = \frac{\phi \text{veCe}}{\phi \text{vrCr}} = \alpha \frac{\phi \text{ve}}{\phi \text{vr}} = S$ 

NB// for single stage

$$S = \frac{Vs}{Vr}$$

Non extracted fraction =  $1 - f = \frac{Cr}{Cf} = \frac{1}{1 + S}$ 

Where f=extracted fraction

 $f = \frac{\text{amount extracted}}{\text{amount in feed}} = \frac{\phi \text{veCe}}{\phi \text{vfCf}}$ 

Therefore for only 1 stage,  $f = \frac{S}{S+1}$ 

For multistage:

$$N = \frac{\ln\left[\left(\frac{S-1}{1-f}\right) + 1\right]}{\ln S} - 1$$

REFRIGERATION CHILLING AND FREEZING

Plank's equation

$$t_f = \left[\frac{\left(\rho \Delta H_L\right)}{\left(T_f - T_a\right)}\right] \left[\left(\frac{2 \operatorname{Pr}}{h}\right) + \left(\frac{4 R r^2}{\lambda}\right)\right]$$

 $\Delta H_L$ = the latent heat of crystallisation of ice (334kJ/kg)

### Shape factors

	Shape		
	Sphere	Infinite Plate	Infinite Cylinder
Shape factor	P=1/6, R=1/24	P=1/16, R=1/24	P=1/16, R=1/24

### Pham's equation

$$t_f = \frac{1}{E} \left[ \left( \frac{\Delta H_1}{\Delta T_1} \right) + \left( \frac{\Delta H_2}{\Delta T_2} \right) \right] \left[ \left( \frac{r}{h} \right) + \left( \frac{r^2}{2\lambda} \right) \right]$$

$$\Delta T_1 = 0.5(T_i + T_{fin}) - T_a$$

$$\Delta T_2 = T_{fm} - T_a$$

$$\Delta H_1 = \rho C_{pu}(T_i - T_{fin})$$

$$\Delta H_2 = \rho \Delta H_L + \rho C_{pf} (T_{fm} - T_{fin})$$

$$T_{fm} = 1.8 + 0.263 T_{fm} + 0.105 T_a$$

$$E = 1 + \left[ \frac{\left(1 + \left(\frac{2}{\beta_i}\right)\right)}{\left(\beta_i^2 + \left(\frac{2\beta_i}{\beta_i}\right)\right)} + \left(\frac{\left(1 + \left(\frac{2}{\beta_i}\right)\right)}{\beta_2^2 + \left(\frac{2\beta_2}{\beta_i}\right)}\right) \right]$$

The shape  $\beta_1 = A/(\pi r^2)$  $B_2 = 3V/(4\pi\beta_1 r^3)$  $B_i=(hr)/\lambda$ , Biot number

### SEDIMENTATION

$$u = \frac{\left[d_{st}^2(\rho_s - \rho)g\right]}{18\mu}$$

### **FILTRATION**

$$\frac{\delta V}{\delta t} = \frac{(A\Delta P)}{R}$$

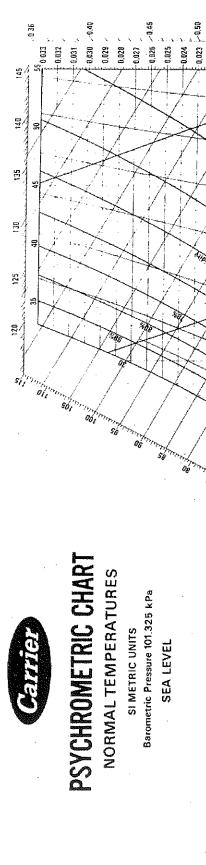
$$R = \mu w(L_c + L)$$

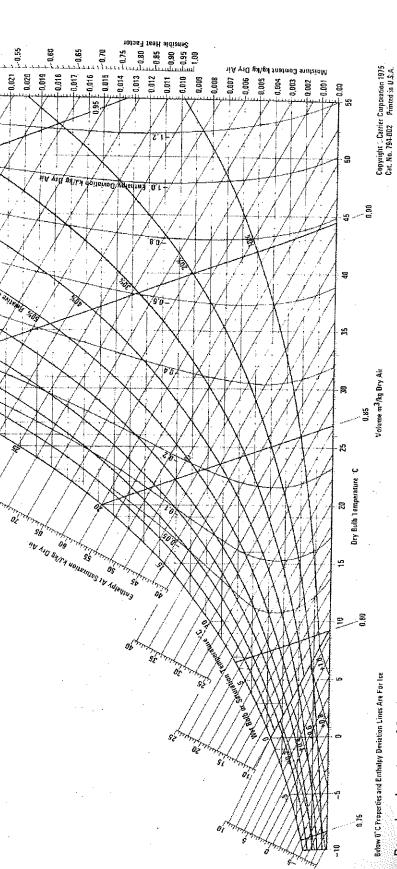
$$L_c = \frac{wV}{A}$$

$$R = \mu w \left[ w \left( \frac{V}{A} \right) + L \right]$$

$$\frac{\delta V}{\delta t} = \frac{A\Delta P}{\mu r \left[w\left(\frac{V}{A}\right) + L\right]}$$
$$\Delta P = \frac{V}{At} \times \mu r \left[w\left(\frac{V}{A}\right) + L\right]$$

$$\Delta P = \frac{V}{At} \times \mu r \left[ w \left( \frac{V}{A} \right) + L \right]$$





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